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Measurement Needs for Fire Safety: Proceedings of an International Workshop

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FORUM Workshop on Measurement Needs for Fire Safety NIST, Gaithersburg, MD April 4-7, 2000

Heat Release Rate (HRR)

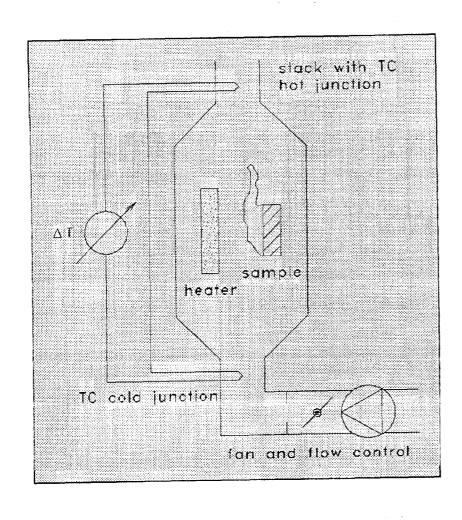
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Outline

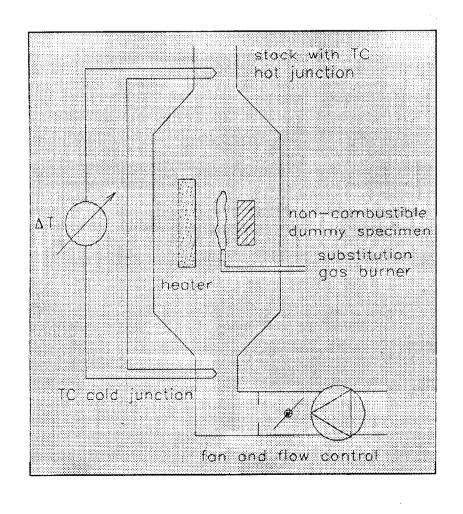
- Methods for measuring heat release rate
 - ➤ Sensible enthalpy rise method
 - ➤ Substitution method
 - ➤ Compensation method
 - Oxygen consumption method
- Heat release rate data and fire modeling
- Uncertainty Analysis
 - ➤ Terminology
 - ➤ Uncertainty of HRR measurements
- Conclusions

Sensible Enthalpy Rise Method



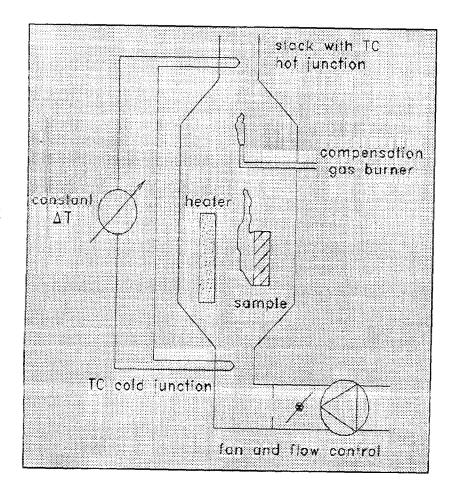
- Examples
 - ➤ Smith (OSU)
- Advantages
 - **➤** Simple
 - **➤** Inexpensive
- Disadvantages
 - ➤ Thermal lag
 - ➤ Radiative fraction

Substitution Method



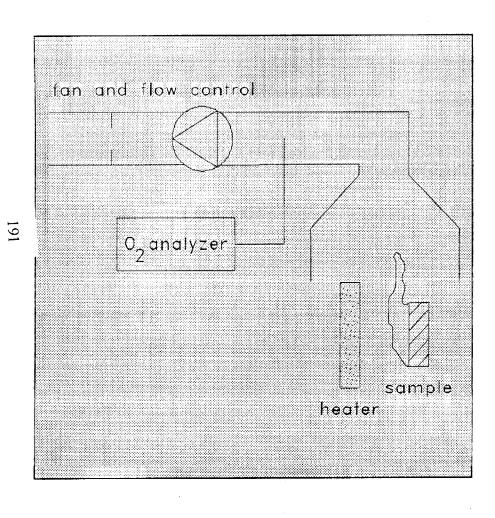
- Examples
 - ➤ Thompson/Cousins (FM)
 - ➤ Brenden (FPL)
- Advantages
 - ➤ No thermal lag problems
- Disadvantages
 - ➤ Complex control system
 - ➤ Double # of tests

Compensation Method



- Examples
 - ➤ Parker/Long (NBS)
 - ➤ Tordella (NBS)
- Advantages
 - ➤ No thermal lag
- Disadvantages
 - ➤ Very complex

Oxygen Consumption Method



Examples

- ➤ Cone calorimeter
- > SBI
- ➤ Room-corner test
- > Furniture calorimeter
- > ICAL
- ➤ Large-Scale calorimeter

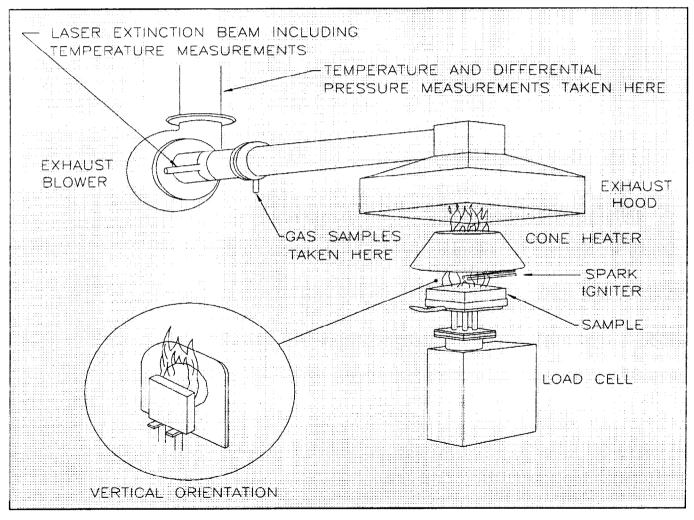
Advantages

- > Practical
- ➤ Accuracy

Disadvantages

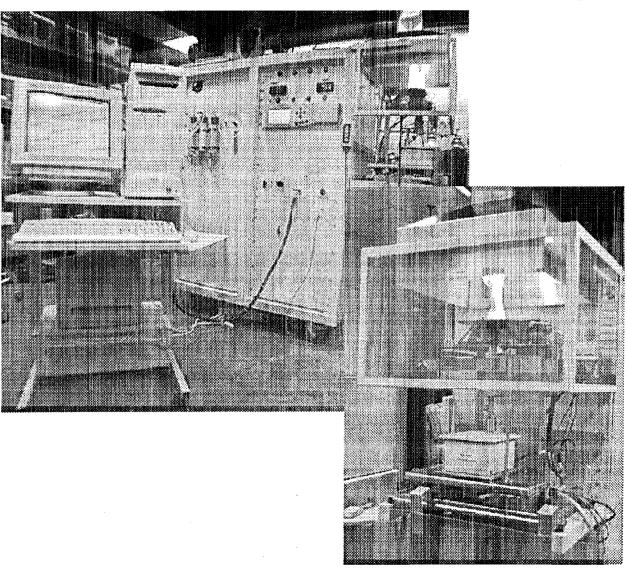
➤ Instrumentation

Small-Scale HRR Testing

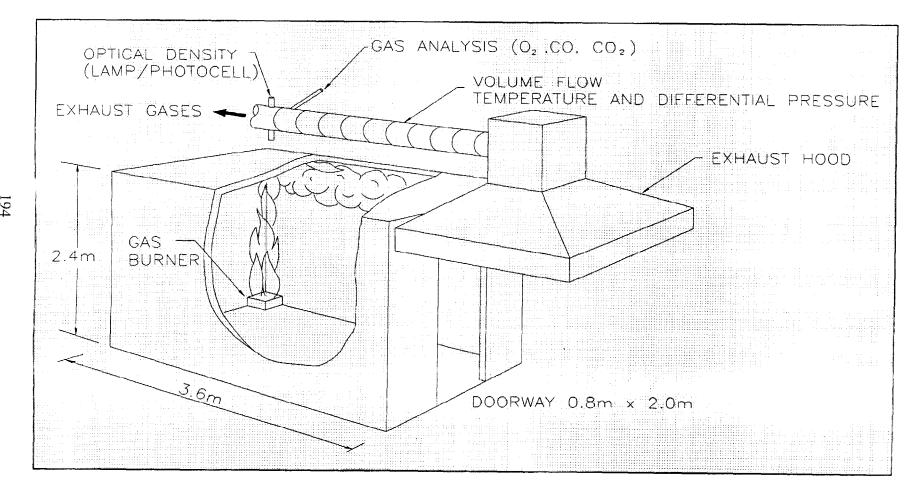


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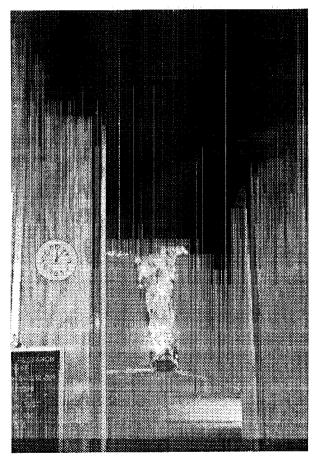
Small-Scale HRR Testing



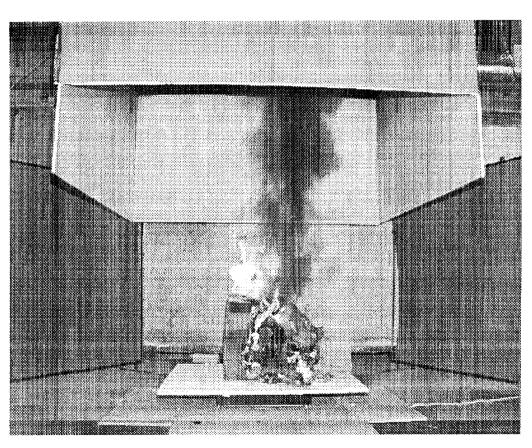
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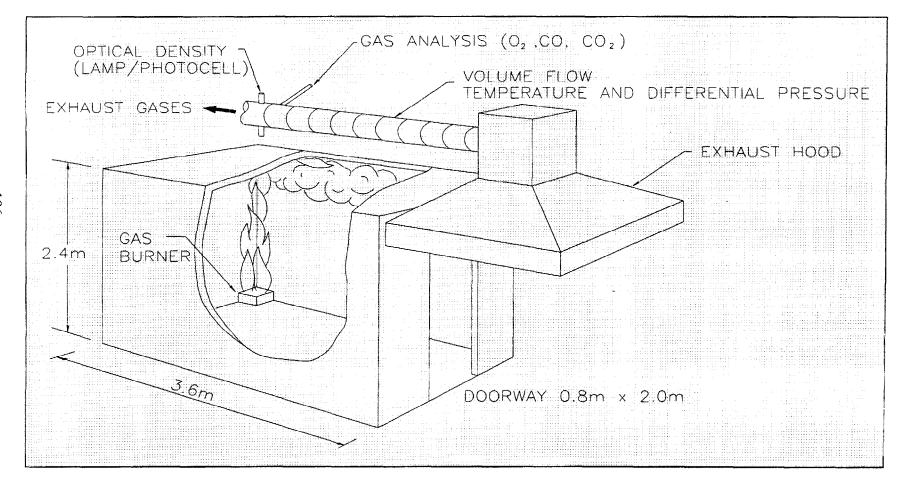
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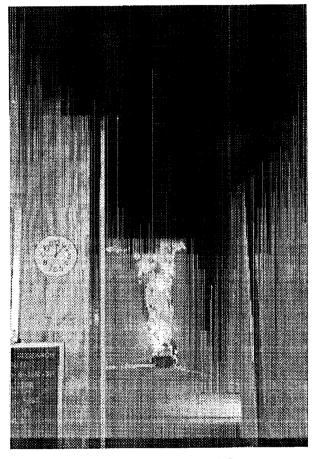
Room-Corner Test



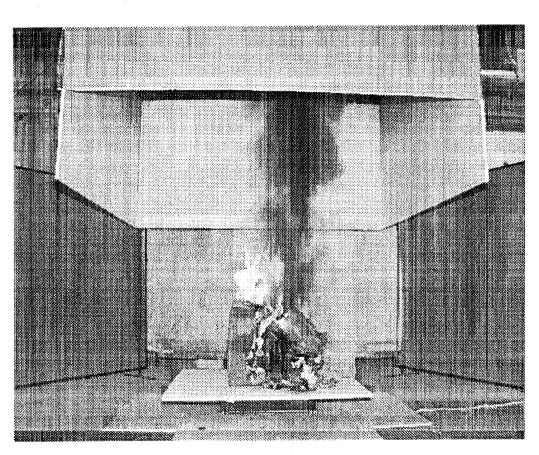
Furniture Calorimeter



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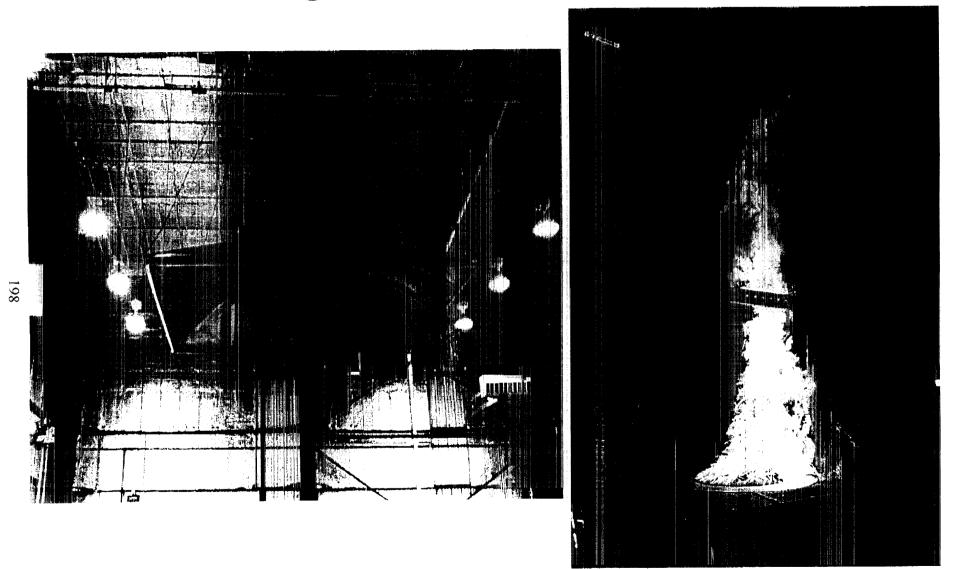


Room-Corner Test



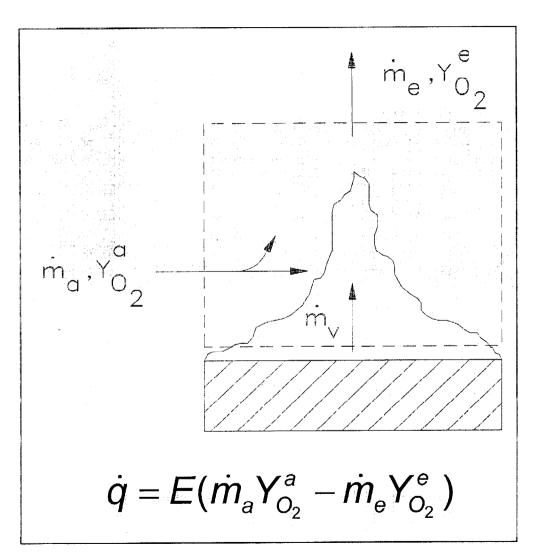
Furniture Calorimeter

Large-Scale Calorimeter



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Oxygen Consumption Method



Oxygen Consumption Method

$$\dot{q} = E \frac{\varphi}{1 + \alpha(\varphi - 1)} C \sqrt{\frac{\Delta P}{T_e}} \frac{M_{O_2}}{M_a} X_{O_2}^a \qquad \text{with} \qquad \varphi = \frac{X_{O_2}^{A^a} - X_{O_2}^{A^e}}{(1 - X_{O_2}^{A^e}) X_{O_2}^{A^a}}$$

$$\phi = \frac{X_{O_2}^{A^a} - X_{O_2}^{A^e}}{(1 - X_{O_2}^{A^e})X_{O_2}^{A^a}}$$

- Equations need to be modified if CO₂ is measured
- Equations can be corrected for CO and soot
- More accurate calculations can be made if water vapor is measured

HRR and Fire Modeling

	Model Input	Model Evaluation
Small-scale data	X	
Intermediate-scale data	X	X
Large-scale data		X

Uncertainty Analysis – Terminology

- Accuracy: Agreement between a measured value and the true value
- Error: Difference between the measured value and the true value, consisting of
 - → Bias error: Fixed or systematic component
 - → Precision error: Random component equal to r + R
- Uncertainty: Interval around the measured value within which the true value lies with C% probability

$$X_{true} = X_{measured} \pm U = X_{measured} \pm \sqrt{U_p^2 + U_b^2}$$

Uncertainty of HRR Measurements

$$\dot{q} = f(E, \alpha, X_{O_2}^{A^e}, X_{O_2}^{A^a}, C, \Delta P, T_e, \dots)$$

$$U_{q} = \sqrt{\left(\frac{\partial f}{\partial E}U_{E}\right)^{2} + \left(\frac{\partial f}{\partial \alpha}U_{\alpha}\right)^{2} + \dots}$$

- Small-scale HRR: U = 5% (Enright/Fleischmann, 1999)
- Large-scale HRR: U = 7% (Dahlberg, 1994)

Uncertainty of HRR Measurements

- Bias can be partially eliminated by calibration
 - Uncertainty of calibration standard
 - 7 Test conditions different from calibration conditions
- Precision uncertainty from round robins

	Year	Labs	Levels	Peak HRR		Total HR	
				r (%)	R(%)	r(%)	R(%)
Cone calorimeter	2000	4	16	17	23	8	15
SBI	1997	16	30	38	54	47	71
ICAL	1999	3	8	56	67	72	118
Room	1994	12	5	65	79	25	41

Uncertainty of HRR Measurements

Discrepancies between uncertainty analyses and round robin data:

- Sample variability
- Operator variability
- Heat flux variability (small-scale)
- Random effects on fire growth (intermediate and large-scale)
- Dynamic errors

Conclusions

- HRR is the primary measure of fire hazard
- HRR is an essential input to fire models
- Databases of HRR data need to be expanded
- Measurement uncertainties need to be reported
- Uncertainties need to be reduced
 - → Proficiency and training programs